Confinement in TFTR and Alternative Approaches to Ignition

TFTR

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Abstract

One of the main conclusions drawn from the experiments in TFTR, and other tokamaks with neutral beam heating, is that energetic ions are very well confined in the core of conventional tokamaks. In TFTR, this was first apparent in the Supershot regime, where the ion temperature approached the convective limit, and, more recently, in the Enhanced Reversed Shear regime where the ion transport approached neoclassical levels. Experiments with ICRF heating and the fusion alpha particles in D-T plasmas support the conclusion. This suggests that it may be possible to approach D-T ignition with substantially lower electron confinement and somewhat lower total plasma pressure than normally considered necessary. Such an alternative was first discussed by Clarke [J.F. Clarke, Nuclear Fusion, **20** (1980) 563]. Indeed, as predicted then, the plasma conditions (density and temperatures) necessary for hot-ion ignition were approached in TFTR, although the confinement was still too low to permit alpha particle heating to dominate. Aspects of the confinement scaling and future possibilities will be presented.



Conventional Approaches to Ignition Are Too Expensive

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ITER design based on sawtoothing, ELMy H-mode scaling:

$$\tau_{\text{E}} \propto H \cdot I_{\text{p}} \cdot R^2 \cdot P^{\text{-0.5}}$$

- Fusion power requirement (~1GW) set by nuclear mission
- Negative power dependence must be offset by large plasma current
- Confinement characteristics of H-mode ($\chi_I \approx \chi_e$) mean $T_I < T_e$
 - alpha particles heat electrons preferentially
 - More β in non-reacting electrons
- High density in edge region (H-mode barrier) where T_I below optimum
- Sawtooth relaxations prevent peaking of pressure profile
- ⇒ Poor ratio of fusion power to square of volume-average plasma pressure



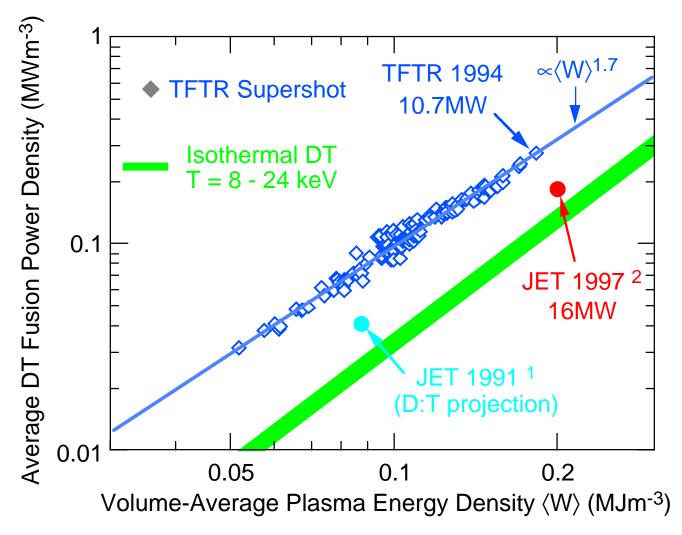
Ignited Plasmas with $T_i > T_e$ are Possible and Interesting

- Success of hot-ion operation with neutral beam heating in PLT (H. Eubank et al., Proc. 7th IAEA Conf., Innsbruck,1978)
- J.F. Clarke investigated the possibility of ignition with T_I > T_e (Nucl. Fusion 20 (1980) 563
 - neoclassical ions: $\tau_{Ei}[s] = 0.73 I_p[MA]^2 T_I[keV]^{1/2} n_i[10^{20} m^{-3}]^{-1}$
 - Alcator scaling for electrons: $\tau_{Ee}[s] = 0.76 \text{ a}[\text{m}]^2 \text{ n}_e[10^{20}\text{m}^{-3}]$
 - → nτ for ignition reduced by factor ~2 with T_i ≈ 30keV; T_e ≈ 25keV
 - \Rightarrow Improved thermal stability at ignition *but* penalties on β_{α}
 - ⇒ Further improvement by "channeling" alpha energy directly to ions
- Discovery of L-mode scaling in early 1980's quelled enthusiasm
 - both electrons and ions worse than originally hoped but
 - hot-ion modes continued to produce the best fusion performance



Hot-Ion Plasmas Have High Reactivity

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¹Nuclear Fusion **32** (1992) 187; ²Phys. Plasmas **5** (1998) 1839



Comparison of Achieved Plasma Parameters with ITER

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Central values	ITER ¹	TFTR	JET ²	JT-60U ³
Plasma composition	DT	DT	DT	D
Mode	ELMy H-mode	Supershot	Hot-ion ELM- free H-mode	Reversed-shear High-β _P
n _e [10 ²⁰ m ⁻³]	1.3	1.02	0.42	0.85
n _{DT} [10 ²⁰ m ⁻³]	8.0	0.60	0.35	0.48 (n _i)
n _{He} [10 ²⁰ m ⁻³]	0.2	0.002		
T _i [keV]	19	40	28	16
T _e [keV]	21	13	14	7
Z _{eff}	1.8	1.8	2.1	3.2
p _{tot} [MPa]	0.8	0.75	0.37	0.22
P_{α} [MWm ⁻³] (source)	0.5	0.45	0.14	
P _{aux} [MWm ⁻³]	0	3.4	0.8	0.3

¹ ITER Final Design Review Document

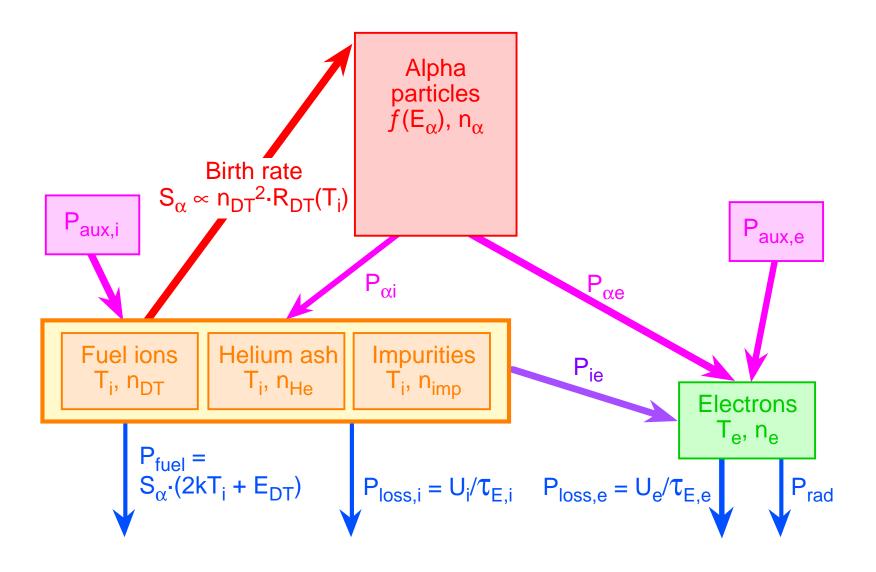
• Confinement and pulse length are the remaining issues!



² A. Gibson *et al.* Phys. Plasmas **5** (1998) 1839

³ S. Ishida *et al.*, paper IAEA-CN-69/OV1/1, IAEA Fusion Energy Conference, Yokohama, Oct. 1998

Power Flow in an Ignited Plasma





Steady-State Power Balance in Self-Heated Plasma

•
$$0 = P_{\alpha i} + P_{aux,i} - P_{ie} - P_{fuel} - \frac{U_i}{\tau_{Ei}}$$

•
$$0 = P_{\alpha e} + P_{aux,e} + P_{ie} - P_{rad} - \frac{U_e}{\tau_{Fe}}$$

•
$$P_{\alpha} = P_{\alpha i} + P_{\alpha e} = E_{\alpha 0} \cdot n_D \cdot n_T \cdot \langle \sigma_{DT} \cdot v \rangle_{T_i}$$

•
$$\frac{dE_{\alpha}}{dt} = -(v_E^{(\alpha e)} + \sum_i v_E^{(\alpha i)}) E_{\alpha}$$
 Integrate from birth to thermal assuming perfect confinement

Integrate from birth to thermal energy

•
$$v_E^{(\alpha e)} = 10.1 \cdot \lambda_{\alpha e} \cdot n_e \cdot T_e^{-3/2} \cdot (1 - \frac{3}{2} T_e / E_{\alpha})$$

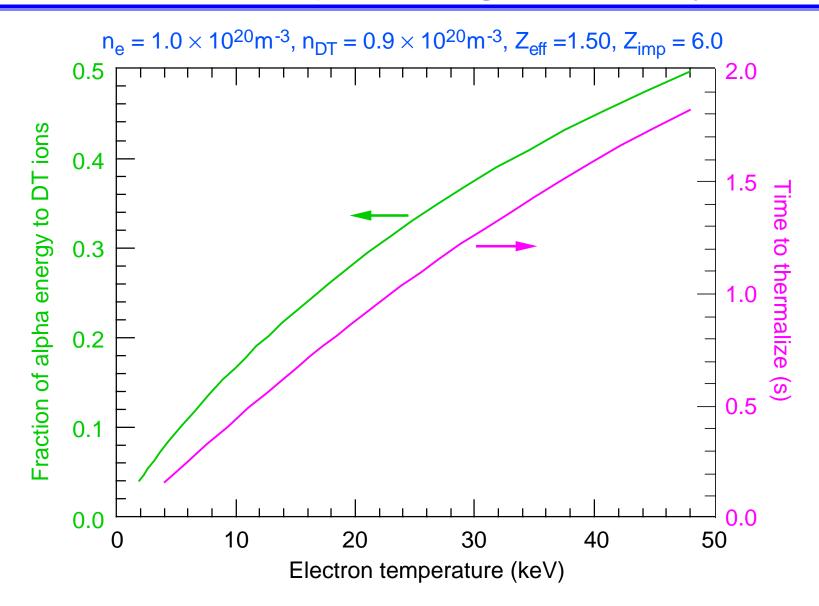
•
$$v_E^{(\alpha i)} = 4.6 \times 10^3 \cdot \lambda_{\alpha i} \cdot \frac{Z_i^2}{A_i} n_i \cdot E_{\alpha}^{-3/2} \cdot \mathbf{F}_i (E_{\alpha} / T_i); \ \mathbf{F}_i \sim 1 \ [\text{s}^{-1}; 10^{20} \text{m}^{-3}; \text{keV}]$$

•
$$P_{ie} = 0.24 \cdot \lambda_{ie} \cdot \frac{(T_i - T_e)}{T_e^{3/2}} \cdot n_e \cdot \sum_i \frac{Z_i^2}{A_i} n_i$$
 [MWm⁻³; keV; 10²⁰m⁻³]

• P_{α} and $P_{ie} \propto n^2 \Rightarrow T_I/T_e$ independent of density



Substantial Direct Alpha Heating of Ions for T_e > 15 keV



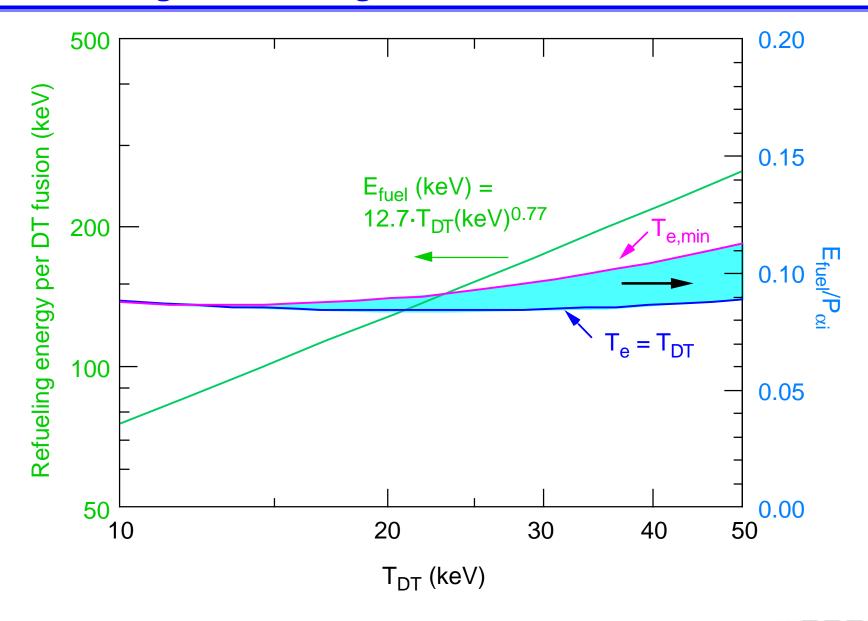


Good Alpha Confinement Essential for Ion Heating

 $T_e = T_i = 20 \text{keV}; n_e = 1.0 \times 10^{20} \text{m}^{-3}, \text{ H:D:T=0.06,0.47,0.47}; Z_{eff} = 1.50$ 10⁰[Normalized alpha energy Ecrit 10-1 Fraction of alpha heating to ions 10-2 0.2 0.3 0.0 0.1 0.4 0.5 0.6 0.7 8.0 0.9 Time (s)



Refueling Power is Significant in Self-Heated Plasmas



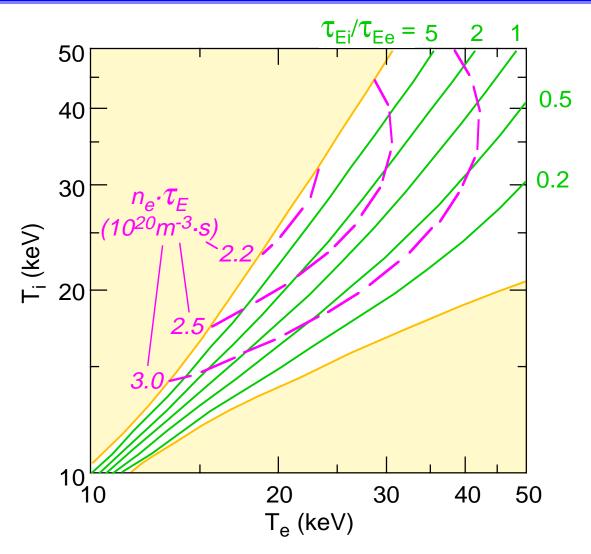


0-D Solutions of Power Balance Equations

- Fix composition of isothermal, isobaric plasma:
 - n_{DT} : n_{H} : n_{He} : n_{C} = 0.80 : 0.05 : 0.05 : 0.01
 - based on TFTR experience with addition of helium ash
- Choose global Q and partition of auxiliary heating, P_{aux,i}, P_{aux,e}
- Scan through T_i, T_e space, calculating self-consistently
 - DT reaction rate
 - Alpha heating terms $P_{\alpha i}$, $P_{\alpha e}$, unthermalized alpha density n_{α} , β_{α} , n_{e}
 - Ion-electron coupling P_{ie}, refueling power P_{fuel}
 - Conducted power and implied confinement time
- Calculate limits of accessible region and contours of $n\tau$, $\beta_{\alpha}/\beta_{tot}$ etc.



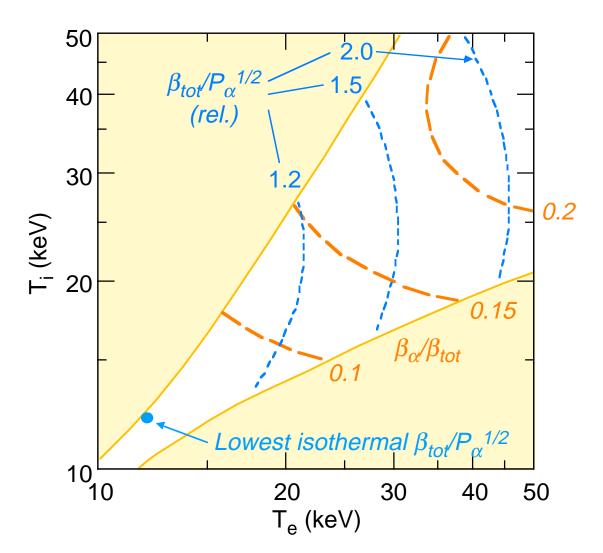
Good Ion Confinement Produces Hot-Ions at Ignition



• Total $n\tau$ requirement reduced by improving ion confinement



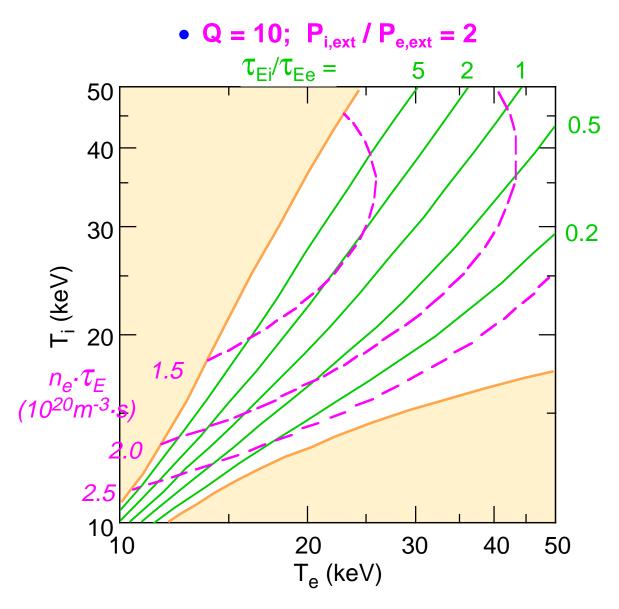
Penalty is Higher β_{tot} and $\beta_{\alpha}/\beta_{tot}$



 \bullet Cannot simultaneously minimize $n\tau$ and β_{tot} at ignition



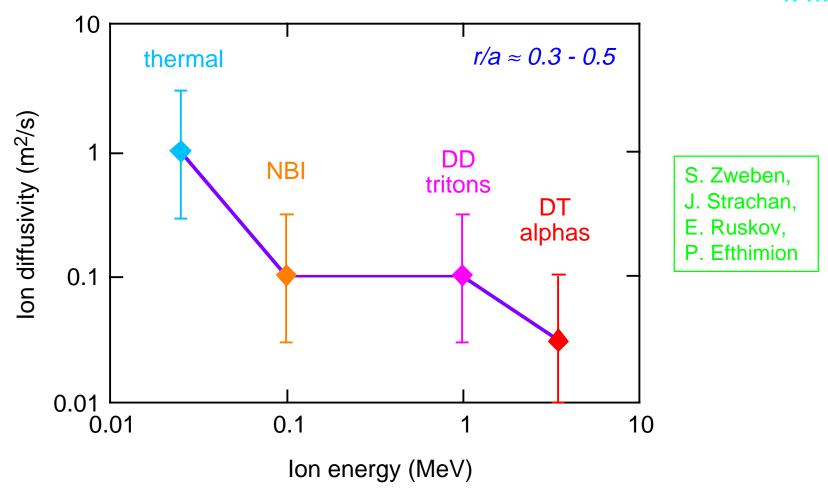
Regime Expands for High-Q with Preferential Ion Heating





Apparent Ion Diffusivity Decreases with Ion Energy in TFTR

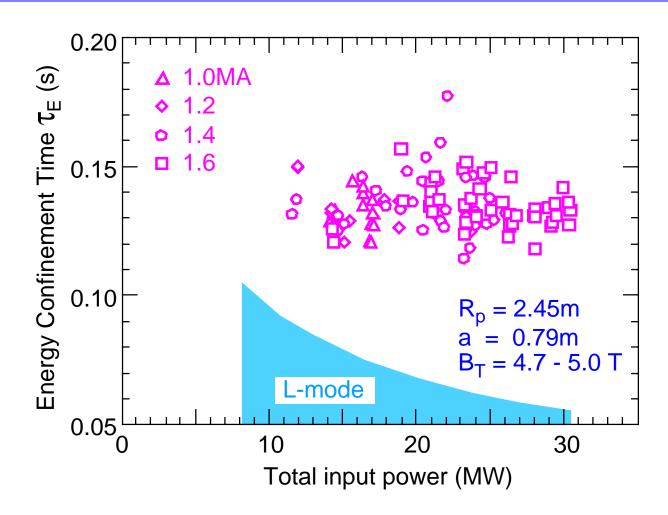
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 Diffusivity for alphas is probably adequate for achievement of hot-ion ignited regime.



Supershot Confinement does not Degrade with Power

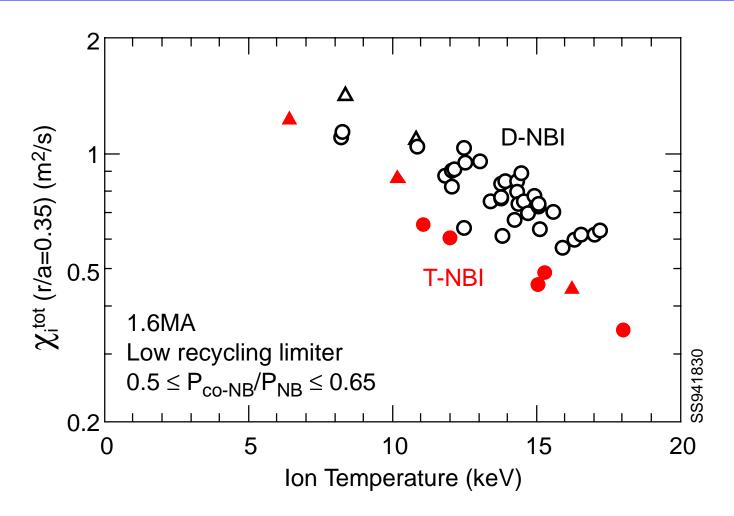


- Confinement dependent on "non-traditional" scaling parameters
 - created difficulties for comparing tokamaks to develop scaling



Ion Thermal Diffusivity Appears to Decreases with T₁

TFTR

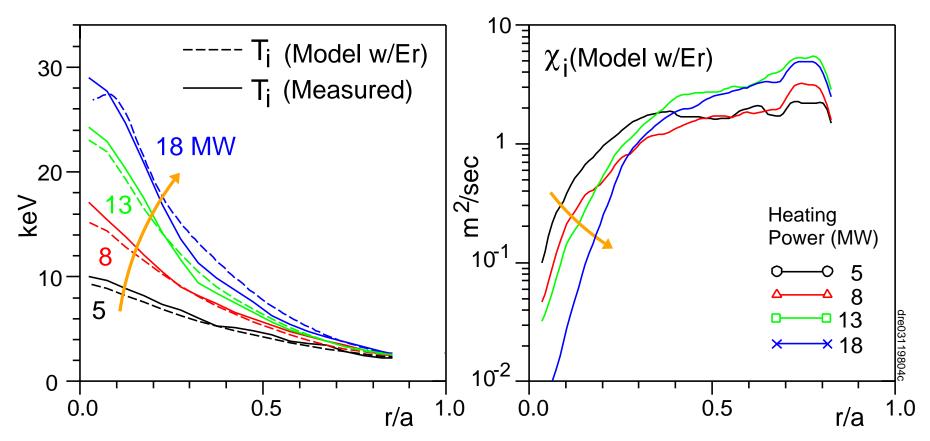


 Both temperature and mass dependence are favorable and not consistent with naïve expectations of Bohm or gyro-Bohm scaling



Model for Suppression of ITG Turbulent Transport by Self-Consistent Plasma Flow Reproduces Behavior of $\chi_{\rm I}$

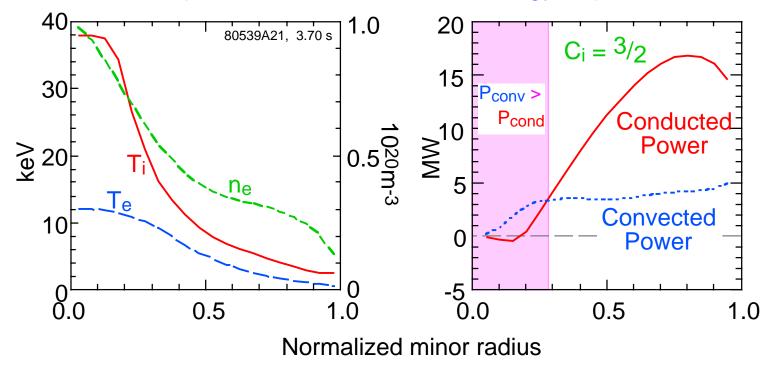
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• Favorable apparent dependence of χ_l on T_l and broadening of region of reduced transport as heating power increased (*D.R. Ernst, this conference*)



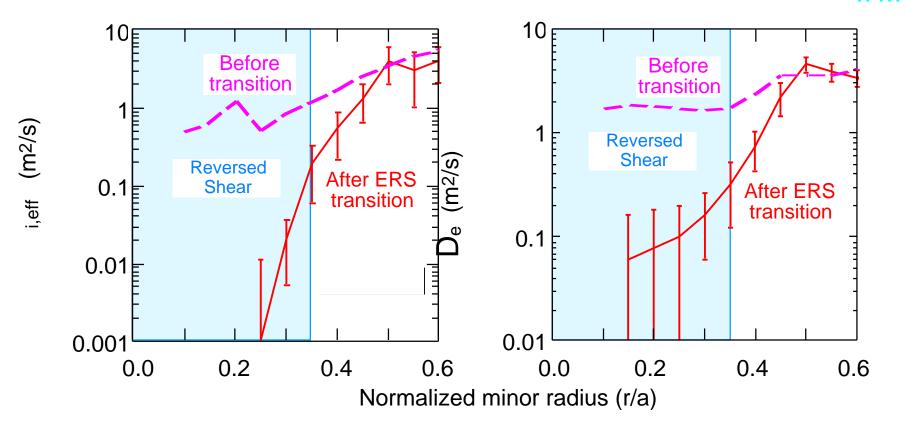
- Ion thermal flux: $q_i = -n_i \chi_i k \nabla T_i + CkT_i \Gamma_i$; Γ_i = particle flux
 - $C = \frac{5}{2}$ for uniform losses (= average particle energy + p.dV work)
 - C = ³/₂ for supershots consistent with energy dependence of D_i



- Convective losses probably too high in standard supershots to ignite, but
 - Balance of conduction and convection in core not well determined



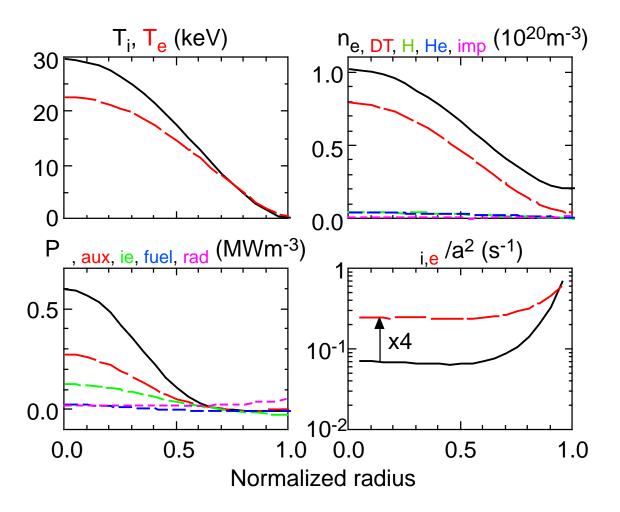
ERS Plasmas Combine Low with Greatly Reduced De



- Flux balance effective : $q = -n \cdot _{eff}$. T (includes convected heat flow)
- e reduced near q_{min} but *increased* inside (M. Zarnstorff, this conference)



Construct Simple 1-D Solution for a Hot-Ion Q = 10 Plasma



• $<P_{fus}> 0.45 \text{ MWm}^{-3} \text{ (ITER: 0.75)};$ _E = 2.7 s (ITER: 5.8 s for ignition)



Embodiment of a Hot-Ion Q = 10 Plasma

- From 1-D calculation: $= \frac{2}{3} (<P > + <P_{aux}>)$ E = 0.25 MPa
- Choose moderately conservative assumptions
 - Inverse aspect ratio: = 1/3
 - Elongation: b/a = = 1.6
 - Engineering safety factor: $\mathbf{q_e} = (/\mu_0) (1 + ^2)$ a B / I = 3
 - Troyon-normalized-: $_{N} = 10^{8} < > a B / I = 80 a / B I = 2$
- Calculate
 - Toroidal field: B = 5.6 T
 - Ratio of plasma current to minor radius: I / a = 5.5 MAm⁻¹
 - For a = 1.5m, R = 4.5m, I = 8.2MA $P_{fus} = 150MW$, $P_{aux} = 15MW$
 - $H_{ITER-89P} = 3.4$
 - Would need $_{i} \sim 0.2 \text{ m}^{2}\text{s}^{-1}$ and $_{e} \sim 0.8 \text{ m}^{2}\text{s}^{-1}$ for r/a < 0.6
- This is within the bounds of what might be achievable



Conclusions and Future Directions

- We should re-examine approaches to ignition in regimes than the "traditional" (i.e. since ca. 1985) ELMy H-mode route
- Hot-ion regimes have produced the best performance in all large tokamaks and are not incompatible with high-Q and, possibly, ignition in DT
- Hot-ion regimes are thermally stable at ignition
 - probable natural operating point for uncontrolled burn
- Study hot-ion regimes per se in other large tokamaks
 - mechanism: sheared flow, T_i/T_e > 1, L_n
 - is strong central fueling necessary?
 - MHD stability margins
 - size scaling in comparable regimes

 controlled experiments
 - put effort into controlling what matters
 - investigate alpha channeling

← theory progress

← reduced D regimes

← optimize r.m.s. pressure

← edge control

